

Exam in Antenna Theory

Time: 31 March 2008, at 8.00–13.00.

Location: Polacksbacken, Skrivalsal

You may bring: Laboratory reports, pocket calculator, English dictionary, Råde-Westergren: "Beta", Nordling-Österman: "Physics Handbook", or comparable handbooks.

Six problems, maximum five points each, for a total maximum of 30 points.

1. Consider an infinitesimal electric dipole of length l placed symmetrically at the origin. Assume that the current in the dipole is constant and given by $\mathbf{I}_e(z') = \hat{\mathbf{z}} I_0$. Find the electric and magnetic field components radiated by the dipole in *all* space.

Hints: The vector potential \mathbf{A} is given by

$$\mathbf{A} = \frac{\mu}{4\pi} \int \mathbf{I}_e(x', y', z') \frac{e^{-jkR}}{R} dl'$$

where R is the distance from any point on the source to the observation point. The magnetic and electric fields are given by

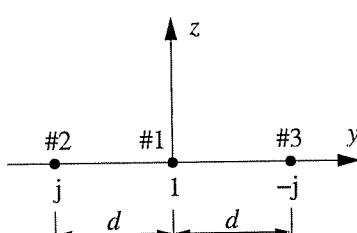
$$\begin{aligned}\mathbf{H} &= \frac{1}{\mu} \nabla \times \mathbf{A} \\ \mathbf{E} &= -j\omega \mathbf{A} - j \frac{1}{\omega \mu \epsilon} \nabla (\nabla \cdot \mathbf{A}) = \frac{1}{j\omega \epsilon} \nabla \times \mathbf{H}\end{aligned}$$

2. The directivity and the effective area are two parameters describing the performance of an antenna in the transmitting and receiving mode respectively. Reciprocity requires that there must be a relation between these parameters.

- a) Derive this relation for a lossless, impedance-matched and polarisation-matched antenna.
- b) Generalize your derived formula by taking into account the antenna radiation efficiency, the reflection efficiency and the polarization loss factor.

Hint: Consider two antennas separated by a distance R and find the relation between the directivities and effective areas of the antennas. Then, use that the maximum effective area of an isotropic source is $(A_{em})_{isotropic} = \lambda^2/(4\pi)$

3. A three element array of isotropic sources placed along the y axis has the phase and magnitude relationships shown in the figure below. For a spacing $d = \lambda/4$, derive the array factor of the array.



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4. An infinitesimal horizontal electric dipole of length l is placed parallel to the x axis at a height h above an infinite electric ground plane. Find the smallest height h (excluding $h = 0$) that the antenna must be elevated so that the far-field pattern has a null in the $\phi = 30^\circ$ plane at an angle of $\theta = 45^\circ$ from the vertical axis.

Hint: The far-field components radiated from an infinitesimal electric dipole, of length l , placed symmetrically about the origin and directed along the z axis are given by

$$\begin{aligned}\mathbf{E} &= \hat{\theta} E_\theta, \quad \text{where } E_\theta = j\eta \frac{k l_0 l}{4\pi r} e^{-jkr} \sin \theta, \\ \mathbf{H} &= \hat{\phi} H_\phi, \quad \text{where } H_\phi = E_\theta / \eta.\end{aligned}$$

5. Design a constant current circular loop so that its pattern has a null in its far-field pattern at $\theta = 30^\circ$. Find the

- a) smallest possible radius of the loop;
- b) angles where the nulls of the far-field pattern occur.

Hint: The far-field components radiated by a circular loop of constant current I_0 are given by

$$\begin{aligned}E_\phi &= \frac{a\omega\mu I_0}{2r} e^{-jkr} J_1(ka \sin \theta), \\ H_\theta &= -E_\phi / \eta,\end{aligned}$$

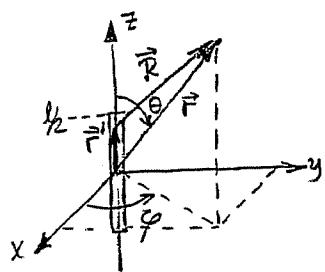
where a is the radius of the loop and $J_1(z)$ is the Bessel function of the first order. Nulls of the Bessel function [$J_1(z_n) = 0$] occur at $z_1=0, z_2=3.87, z_3=7.08, z_4=10.17, \dots$

6. A linear array of isotropic sources is placed along the z axis with the distance $d = \lambda/4$ between the elements. By setting $z = e^{j\psi}$, where $\psi = kd \cos \theta + \beta$, the array factor of the array can be written as

$$AF = \sum_{n=1}^N a_n e^{j(n-1)\psi} = \sum_{n=1}^N a_n z^{n-1} = (z-1)(z-j)(z+1)$$

- a) Determine the progressive phase shift β so that the array factor has three nulls.
- b) For your choice of β , sketch and label the visible region on the unit circle.

1



$$\vec{A} = \frac{\mu}{4\pi} \int_C \vec{I}_e(x', y', z') \frac{e^{-jkR}}{R} dV'$$

Infinitesimal dipole $\Rightarrow \vec{I}_e = \hat{a}_z I_0$

$R = r - r'$ $r' = (x', y', z') = \vec{r}'$ for infinitesimal dipole

$R = \vec{r}$ for phase and amplitude

$$\vec{A} = \hat{a}_z \frac{\mu I_0}{4\pi} \frac{e^{-jkr}}{r} \int_{-l/2}^{l/2} dz' = \hat{a}_z \frac{\mu I_0 l}{4\pi} e^{-jkr}$$

$$\hat{a}_z = \hat{a}_r \cos\theta - \hat{a}_\theta \sin\theta$$

$$\vec{A} = \frac{\mu I_0 l}{4\pi r} e^{-jkr} (\hat{a}_r \cos\theta - \hat{a}_\theta \sin\theta)$$

$$\vec{H} = \frac{1}{\mu} \nabla \times \vec{A} = \frac{1}{\mu} \left\{ \hat{a}_\phi \frac{1}{r} \left[\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right] \right\} \quad \vec{A} = (A_r, A_\theta, 0)$$

$$= \frac{1}{\mu} \hat{a}_\phi \frac{1}{r} \left[\frac{\partial}{\partial r} \left(-\frac{\mu I_0 l}{4\pi} e^{-jkr} \sin\theta \right) - \frac{\partial}{\partial \theta} \left(\frac{\mu I_0 l}{4\pi r} e^{-jkr} \cos\theta \right) \right]$$

$$= \frac{1}{\mu} \hat{a}_\phi \frac{1}{r} \left[\frac{\mu I_0 l}{4\pi} e^{-jkr} (-jk \sin\theta) + \frac{\mu I_0 l}{4\pi r} e^{-jkr} \sin\theta \right]$$

$$= -\hat{a}_\phi \frac{\mu I_0 l}{4\pi r} e^{-jkr} \left[jk \sin\theta + jk \frac{\sin\theta}{jkr} \right]$$

$$= \hat{a}_\phi j \frac{\mu I_0 l}{4\pi r} \sin\theta \left[1 + \frac{1}{jkr} \right] e^{-jkr}$$

$$\vec{E} = \frac{1}{j\omega \epsilon} \nabla \times \vec{H} \quad \vec{H} = (0, 0, H_\phi)$$

$$= \frac{1}{j\omega \epsilon} \left\{ \frac{\hat{a}_r}{r \sin\theta} \left[\frac{\partial}{\partial \theta} (H_\phi \sin\theta) \right] + \frac{\hat{a}_\theta}{r} \left[-\frac{\partial}{\partial r} (r H_\phi) \right] \right\}$$

$$= \frac{1}{j\omega \epsilon} j \frac{\mu I_0 l}{4\pi} \left\{ \frac{\hat{a}_r}{r \sin\theta} \left[\frac{\partial}{\partial \theta} \left(\frac{1}{r} \sin^2 \theta \left[1 + \frac{1}{jkr} \right] e^{-jkr} \right) \right] + \frac{\hat{a}_\theta}{r} \left[-\frac{\partial}{\partial r} \left(\sin\theta \left[1 + \frac{1}{jkr} \right] e^{-jkr} \right) \right] \right\}$$

$$= \frac{1}{j\omega \epsilon} \left\{ \frac{\hat{a}_r}{r \sin\theta} \left[j \frac{\mu I_0 l}{4\pi r} \left[1 + \frac{1}{jkr} \right] e^{-jkr} \frac{\partial}{\partial \theta} (\sin^2 \theta) \right] + \frac{\hat{a}_\theta}{r} j \frac{\mu I_0 l}{4\pi} \sin\theta \left[-\frac{\partial}{\partial r} \left(r \frac{1}{r} \left[1 + \frac{1}{jkr} \right] e^{-jkr} \right) \right] \right\}$$

$$= \frac{1}{j\omega \epsilon} j \frac{\mu I_0 l}{4\pi} \left\{ \frac{\hat{a}_r}{r \sin\theta} \left[1 + \frac{1}{jkr} \right] e^{-jkr} 2 \sin\theta \cos\theta - \frac{\hat{a}_\theta}{r} \sin\theta \left[-jk - \frac{1}{r} - \frac{1}{jkr^2} \right] e^{-jkr} \right\}$$

$$= \frac{k}{\omega \epsilon} \frac{I_0 l}{4\pi} \left\{ \hat{a}_r \frac{2}{r^2} \left[1 + \frac{1}{jkr} \right] e^{-jkr} \cos\theta + \hat{a}_\theta \frac{jk}{r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2} \right] e^{-jkr} \sin\theta \right\}$$

$$= \hat{a}_r \underbrace{\eta \frac{I_0 l \cos\theta}{2\pi r^2} \left[1 + \frac{1}{jkr} \right] e^{-jkr}}_{E_r} + \hat{a}_\theta \underbrace{j \eta \frac{k I_0 l \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2} \right] e^{-jkr}}_{E_\theta}$$

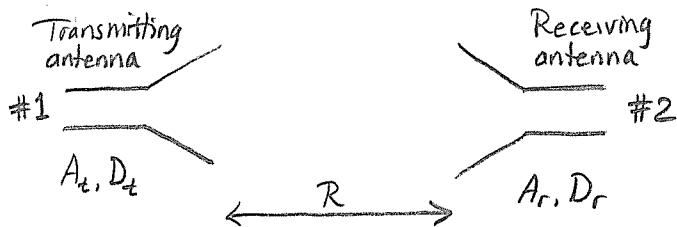
$$H_\phi = j \frac{k I_0 l \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} \right] e^{-jkr}$$

$$H_r = H_\theta = E_\phi = 0$$

$$E_r = \eta \frac{I_0 l \cos\theta}{2\pi r^2} \left[1 + \frac{1}{jkr} \right] e^{-jkr}$$

$$E_\theta = j \eta \frac{k I_0 l \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2} \right] e^{-jkr}$$

2



The power density at a distance R from antenna #1

$$W_t = D_t \frac{P_t}{4\pi R^2} \quad \left(\text{for isotropic } W_0 = \frac{P_t}{4\pi R^2} \right)$$

Power received by antenna #2

$$\begin{aligned} P_r &= A_r W_t = \frac{P_t D_t A_r}{4\pi R^2} \\ \Rightarrow D_t A_r &= \frac{P_r}{P_t} 4\pi R^2 \end{aligned} \quad (1)$$

Now, reverse the situation and let antenna #2 be transmitter and antenna #1 receiver. The power density at the distance R from antenna #2 then becomes

$$W_r = D_r \frac{P_t}{4\pi R^2} \quad \left(\text{for isotropic } W_0 = \frac{P_t}{4\pi R^2} \right)$$

The power received by antenna #1

$$\begin{aligned} P_r &= A_t W_r = \frac{P_t D_r A_t}{4\pi R^2} \\ \Rightarrow D_r A_t &= \frac{P_r}{P_t} 4\pi R^2 \end{aligned} \quad (2)$$

$$(1) = (2) \Rightarrow$$

$$D_t A_r = D_r A_t$$

$$\Rightarrow \frac{D_t}{A_t} = \frac{D_r}{A_r} = \text{const for all antennas}$$

Specifically, for an isotropic source we have $D_0 = 1$, $A_{em} = \frac{\lambda^2}{4\pi}$, so

$$\frac{D}{A} = \frac{1}{\lambda^2/(4\pi)}$$

For maximum directivity and maximum effective area

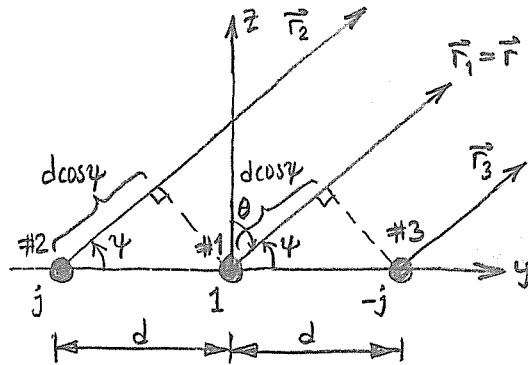
$$A_{em} = \frac{\lambda^2}{4\pi} D_0$$

Taking into account radiation efficiency, impedance-matching, and the PLF:

$$A_{em} = \epsilon_{cd} (1 - |\Gamma|^2) \frac{\lambda^2}{4\pi} D_0 |\hat{s}_w \cdot \hat{s}_a|^2$$

where \hat{s}_w and \hat{s}_a are polarization unit vectors of the wave and the antenna, respectively.

3



$$d = \frac{\lambda}{4}$$

$$kd = \frac{2\pi}{\lambda} \frac{\lambda}{4} = \frac{\pi}{2}$$

$$E = \sum_{n=1}^N a_n \frac{e^{-jkr_n}}{r_n} = a_1 \frac{e^{-jkr_1}}{r_1} + a_2 \frac{e^{-jkr_2}}{r_2} + a_3 \frac{e^{-jkr_3}}{r_3}$$

Far-field approximation: $(r_1 \equiv r)$

$$\left. \begin{array}{l} r_2 \approx r + d \cos \psi \\ r_3 \approx r - d \cos \psi \end{array} \right\} \text{for phases}$$

$r_2 \approx r_3$ for amplitudes

$$AF = 1 + j e^{-jk d \cos \psi} - j e^{jk d \cos \psi}$$

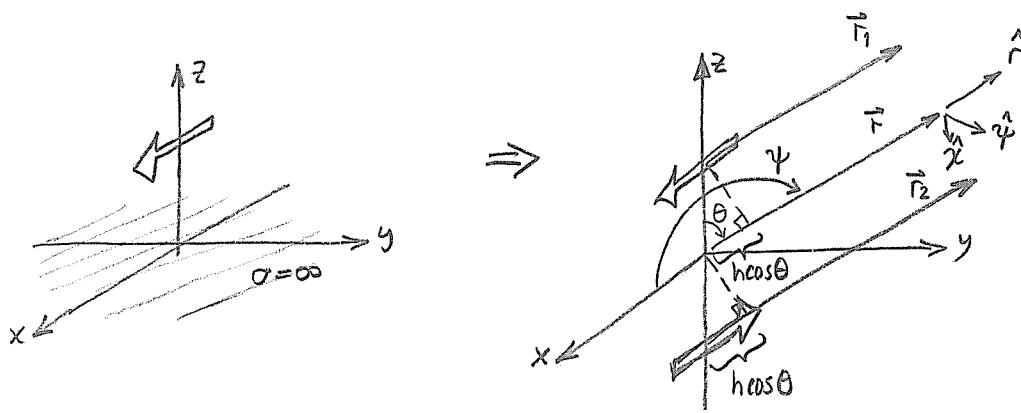
$$= 1 - j \underbrace{(e^{jk d \cos \psi} - e^{-jk d \cos \psi})}_{2j \sin(k d \cos \psi)}$$

$$= 1 + 2 \sin(k d \cos \psi)$$

$$\cos \psi = \hat{y} \cdot \hat{r} = \sin \theta \sin \phi$$

$$AF = 1 + 2 \sin\left(\frac{\pi}{2} \sin \theta \sin \phi\right)$$

4.

Introduce a new spherical coordinate system (r, ψ, χ)

$$E_\psi = E_\psi^d + E_\psi^r \quad \text{where}$$

$$E_\psi^d = j\eta \frac{kI_0 l}{4\pi r_1} e^{-jkr_1} \sin\psi$$

$$E_\psi^r = -j\eta \frac{kI_0 l}{4\pi r_2} e^{-jkr_2} \sin\psi$$

$$\vec{H} = \frac{1}{\eta} \hat{r} \times \vec{E}$$

$$\begin{aligned} \sin\psi &= \sqrt{1 - \cos^2\psi} = \sqrt{1 - |\hat{x} \cdot \hat{r}|^2} \\ &= \sqrt{1 - \sin^2\theta \cos^2\phi} \end{aligned}$$

Far-field approximation

$$\left. \begin{array}{l} r_1 \approx r - h \cos\theta \\ r_2 \approx r + h \cos\theta \end{array} \right\} \text{for phases}$$

$$r_1 \approx r_2 \approx r \quad \text{for amplitudes}$$

$$\begin{aligned} E_\psi &= j\eta \frac{kI_0 l}{4\pi r} e^{-jkr} \sin\psi \underbrace{\left[e^{jkh \cos\theta} - e^{-jkh \cos\theta} \right]}_{2j \sin(kh \cos\theta)} \\ &= j\eta \frac{kI_0 l}{4\pi r} e^{-jkr} \sqrt{1 - \sin^2\theta \cos^2\phi} \left[2j \sin(kh \cos\theta) \right] \end{aligned}$$

Null for $\theta = 45^\circ, \phi = 30^\circ$

$$\Rightarrow \sqrt{1 - \sin^2\theta \cos^2\phi} \sin(kh \cos\theta) \Big|_{\theta=45^\circ, \phi=30^\circ} = 0$$

$$\Rightarrow \sqrt{1 - \sin^2 45^\circ \cos^2 30^\circ} \neq 0 \quad \text{and} \quad \sin(kh \cos 45^\circ) = 0$$

$$\sin\left(\frac{2\pi}{\lambda} h \frac{1}{\sqrt{2}}\right) = \sin\left(\frac{\sqrt{2}\pi h}{\lambda}\right) = 0$$

$$\frac{\sqrt{2}\pi h}{\lambda} = n\pi \quad n = 0, 1, \dots$$

$$n=1 \text{ gives the lowest height } h = \frac{\lambda}{\sqrt{2}}$$

5. The nulls of the Bessel function J_1 are $0; 3.87; 7.08; 10.17; \dots$

The first null gives

$$ka \sin \theta = 0 \Rightarrow \sin \theta = 0 \Rightarrow \theta_1 = 0^\circ \\ \theta_2 = 180^\circ$$

a) The second null gives the smallest radius of the loop when $\theta_3 = 30^\circ$

$$ka \sin 30^\circ = 3.87 \\ \Rightarrow a = \frac{3.87}{k \sin 30^\circ} = \frac{3.87 \lambda}{2\pi \cdot 1/2} = \frac{3.87 \lambda}{\pi} \approx \underline{\underline{1.23 \lambda}}$$

b) The null $\theta_3 = 30^\circ$ gives also $\theta_4 = 180^\circ - 30^\circ = 150^\circ$

The 3rd null gives

$$ka \sin \theta = 7.08 \\ \Rightarrow \sin \theta = \frac{7.08 \lambda}{2\pi a} = \frac{7.08}{2\pi \cdot 1.23} \Rightarrow \theta_5 = 66.2^\circ \\ \theta_6 = 113.8^\circ$$

The 4th null gives

$$\sin \theta = \frac{10.17}{2\pi \cdot 1.23} = 1.31 > 0 \Rightarrow \text{No more nulls}$$

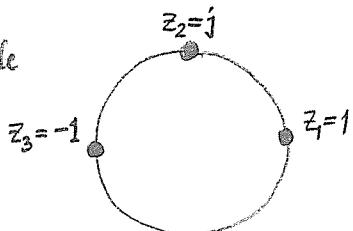
Answer: a) The radius: $a = 1.23 \lambda$

- b) Nulls at $\theta = \begin{matrix} 0^\circ \\ 30^\circ \\ 66.2^\circ \\ 113.8^\circ \\ 150^\circ \\ 180^\circ \end{matrix}$

6. a) The AF has three nulls $z_1 = 1$, $z_2 = j$, $z_3 = -1$ only if all these nulls are within the visible region of the unit circle.

$$z = e^{j\psi}$$

$$|z| = 1 \Rightarrow \text{unit circle}$$



We must choose β so that z_1, z_2, z_3 are within the visible region

$$\psi = kd \cos \theta + \beta = \frac{2\pi}{\lambda} \frac{\lambda}{d} \cos \theta + \beta = \frac{\pi}{2} \cos \theta + \beta$$

$$\theta = 0^\circ \Rightarrow \psi = \frac{\pi}{2} \cos 0^\circ + \beta = \frac{\pi}{2} + \beta$$

$$\theta = 180^\circ \Rightarrow \psi = \frac{\pi}{2} \cos 180^\circ + \beta = -\frac{\pi}{2} + \beta$$

If we choose $\beta = \frac{\pi}{2}$

$$\psi(\theta = 0^\circ) = \pi$$

$$\psi(\theta = 180^\circ) = 0$$

$\Rightarrow z_1, z_2, z_3$ are all within the visible region

For $\beta = 0$:
We must rotate the visible region by choosing $\beta \neq 0$.

b)

